Table II shows that the current measurements supports the relative enthalpy data reported by Yerlett and Wormald (8) over that of Machado and Streett (7), at all temperatures. However, as the temperature increases, the relative enthalpies reported here increase at a faster rate than those reported by Yerlett and Wormald, until at the highest temperature the difference is nearly $6.0 \%$. Yerlett and Wormald report their enthalpy measurements to be accurate to $0.6 \%$. The estimated overall error of the heat capacity measurements in the present measurements is estimated to be $0.9 \%$. While the standard deviation of the data from eq 2 is considerably greater ( $1.65 \%$ ), the error in the enthalpies resulting from the integration of eq 2 will be much smaller. We cannot explain the significant differences between the high-temperature enthalpies calculated from the heat capacities reported in this work and those reported by Yerlett and Wormald.

Registry No. Methanol, 67-56-1.

## Literature Cited

(1) Carison, H. G. Ph.D. Thesis, University of Michigan, Ann Arbor, 1964.
(2) Hough, E. W.; Mason, D. M.; Sage, B. H. J. Am. Chem. Soc. 1950, 72, 5775.
(3) Benson, G. C.; D'Arcy, P. J.; Kiyohara, O. J. Solution Chem. 1980, 9, 931.
(4) Fiock, E. F.; Ginnings, D. C.; Holton, W. B. J. Res. Natt. Bur. Stend. 1931, 6, 881.
(5) Wilhoit, R. C.; Chao, J.; Hall, K. R. J. Phys. Chem. Ref. Data 1985, 14, 1-175.
(6) Toulouklan, Y. S.; Makita, T. Thermophysical Properties of Matter; TPRC Data Series; IFI/Plenum: New York, 1970; Vol. 6.
(7) Machado, J. R. S.; Streett, W. B. J. Chem. Eng. Data 1983, 28, 218.
(8) Yerlett, T. K.; Wormald, C. J. J. Chem. Thermodyn. 1988, 18, 719.
(9) Goodwin, R. D. J. Phys. Chem. Ref. Data 1987, 16, 799.
(10) Lankford, J. I.; Criss, C. M. J. Solution Chem. 1987, 16, 885.
(11) Haar, L.; Gallagher, J. S.; Kell, G. S. NBS /NRC Steam Tables; Hemisphere: New York, 1984.
(12) White D. E.; Wood, R. H. J. Solution Chem. 1982, 11, 223.
(13) Pitzer, K. S.; Peiper, J. C.; Busey, R. H. J. Phys . Chem. Ref. Data 1984, 13,1 .
(14) Desnoyers, J. E.; deVisser, C.; Perron, G.; Picker, P. J. Solution Chem. 1978, 5, 605.
(15) Smith-Magowan, D.; Wood, R. H. J. Chem. Thermodyn. 1981, 13, 1047.
(16) Craven, R. J. B.; de Reuck, K. M. Int. J. Thermophys, 1986, 7, 541.
(17) Griffiths, R. B.; Wheeler, J. C. Phys. Rev. A 1970, 2, 1047.
(18) Sengers, J. V.; Levelt Sengers, J. M. H. Int. J. Thermophys. 1984, 5, 195.

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# Vapor-Liquid Equilibria at $760 \mathbf{m m H g}$ in the Ternary System Methanol-1,1-Dichloroethane-Propyl Bromide 

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#### Abstract

Vapor-liquid equillbrium at atmospheric pressure has been determined for the title ternary system. The data were correlated by varlous equations and the appropriate parameters are reported.


The present work was undertaken to measure VLE data for the ternary system methanol-1,1-dichloroethane-propyl bromide for which no isobaric data are available.

## Experimental Section

Purity of Materlals. Analytical grade methanol (99.5\% + ) was purchased from Frutarom; propyl bromide (99.4\%) and 1, 1-dichloroethane analytical grade $(99.6 \%+)$ were purchased from Merck. The reagents were used without further purification after gas chromatography falled to show any significant impurities. Properties of the pure components appear in Table I.

Apparatus and Procedure. An all-glass modified Dvorak and Boublik recirculation still (1) was used in the equilibrium determination. The experimental features have been described in previous publications (2). All analyses were carried out by gas chromatography on a Packard-Becker Model 417 apparatus provided with a thermal conductivity detector and a Spectra Physics Model SP 4290 electronic integrator. The column was 200 cm long and 0.2 cm in diameter, was packed with $20 \%$ $\mathrm{OV}-17$, and was operated isothermally at $75^{\circ} \mathrm{C}$. Injector and detector temperatures were 220 and $230{ }^{\circ} \mathrm{C}$, respectively. Very good separation was achieved under these conditions, and calibration analyses were carried to convert the peak ratio to the weight composition of the sample. Concentration measurements were accurate to better than $\pm 1 \%$. The accuracy

Table I. Physical Constants of Pure Components

| index | compd | $\begin{gathered} \text { refractive } \\ \text { index } \\ \left(20^{\circ} \mathrm{C}\right) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{bp}(760 \\ \operatorname{mmHg}),{ }^{\circ} \mathrm{C} \end{gathered}$ | purity [GLC (min)] |
| :---: | :---: | :---: | :---: | :---: |
| 1 | methanol | $1.3280^{a}$ | $64.68{ }^{\text {a }}$ | 99.5 |
|  |  | $1.3284^{\text {b }}$ | $64.70^{\text {b }}$ |  |
| 2 | 1,1-dichloroethane | $1.4138^{\text {a }}$ | $57.29^{\text {a }}$ | 99.6 |
|  |  | $1.4135{ }^{\text {b }}$ | $57.28^{\text {b }}$ |  |
| 3 | propyl bromide | $1.4348^{\text {a }}$ | $70.55^{\circ}$ | 99.6 |
|  |  | $1.4343^{\text {b }}$ | $71.0{ }^{\text {b }}$ |  |
|  |  |  | $70.80^{c}$ |  |

${ }^{a}$ Measured. ${ }^{b}$ Reference 12. ${ }^{c}$ Reference 13.
in determination of pressure and temperature was $\Delta P= \pm 2$ mmHg and $\Delta t= \pm 0.02^{\circ} \mathrm{C}$.

## Results

The temperature-concentration measurements at 760 mmHg for the ternary system are reported in Table II together with the activity coefficients which were calculated from the following equation (3)

$$
\begin{array}{r}
\ln \gamma_{1}=\ln \left(P y_{1} / P_{1}{ }^{0} x_{1}\right)+\left(B_{11}-v^{L}{ }_{1}\right)\left(P-P_{1}{ }^{0}\right) / R T+ \\
(P / 2 R T) \sum \sum y_{y_{k}}\left(2 \delta_{j f}-\delta_{j k}\right) \tag{1}
\end{array}
$$

where

$$
\begin{equation*}
\delta_{j l}=2 B_{j}-B_{\| l}-B_{\sharp} \tag{2}
\end{equation*}
$$

Vapor pressures $P_{l}^{0}$ were calculated according to Antoine's equation

$$
\begin{equation*}
\log P_{i}^{0}=\alpha_{t}-\beta_{i} /\left(\delta_{i}+t\right) \tag{3}
\end{equation*}
$$

Table II. Experimental Vapor-Liquid Equilibria Data for Methanol (1)-1,1-Dichloroethane (2)-Propyl Bromide (3) at 760 $\mathbf{m m H g}$

| temp, ${ }^{\circ} \mathrm{C}$ | $x_{1}$ | $x_{2}$ | $x_{3}$ | $y_{1}$ | $y_{2}$ | $y_{3}$ | $\gamma_{1}$ | $\gamma_{2}$ | $\gamma_{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 49.05 | 0.163 | 0.777 | 0.060 | 0.329 | 0.628 | 0.043 | 4.0351 | 1.0626 | 1.4913 |
| 49.51 | 0.376 | 0.563 | 0.061 | 0.329 | 0.624 | 0.047 | 1.7126 | 1.4344 | 1.5771 |
| 49.51 | 0.216 | 0.745 | 0.039 | 0.299 | 0.678 | 0.023 | 2.7109 | 1.1776 | 1.2053 |
| 49.52 | 0.344 | 0.599 | 0.057 | 0.329 | 0.329 | 0.042 | 1.8707 | 1.3587 | 1.5078 |
| 49.54 | 0.248 | 0.714 | 0.038 | 0.316 | 0.660 | 0.024 | 2.4901 | 1.1952 | 1.2908 |
| 49.55 | 0.321 | 0.627 | 0.052 | 0.336 | 0.628 | 0.036 | 2.0436 | 1.2949 | 1.4160 |
| 49.57 | 0.283 | 0.670 | 0.047 | 0.326 | 0.642 | 0.032 | 2.2476 | 1.2378 | 1.3907 |
| 49.58 | 0.363 | 0.575 | 0.062 | 0.336 | 0.617 | 0.047 | 1.8052 | 1.3856 | 1.5485 |
| 49.68 | 0.254 | 0.675 | 0.071 | 0.321 | 0.637 | 0.042 | 2.4547 | 1.2143 | 1.2030 |
| 49.86 | 0.158 | 0.808 | 0.034 | 0.285 | 0.696 | 0.019 | 3.4689 | 1.0990 | 1.1247 |
| 50.07 | 0.381 | 0.519 | 0.100 | 0.365 | 0.555 | 0.080 | 1.8261 | 1.3583 | 1.6080 |
| 50.26 | 0.335 | 0.502 | 0.163 | 0.340 | 0.544 | 0.116 | 1.9221 | 1.3662 | 1.4175 |
| 50.27 | 0.114 | 0.861 | 0.025 | 0.266 | 0.720 | 0.014 | 4.4176 | 1.0542 | 1.1120 |
| 50.34 | 0.542 | 0.394 | 0.064 | 0.439 | 0.495 | 0.066 | 1.5197 | 1.5843 | 2.0641 |
| 50.40 | 0.491 | 0.406 | 0.103 | 0.386 | 0.524 | 0.090 | 1.4751 | 1.6216 | 1.7380 |
| 50.41 | 0.450 | 0.435 | 0.115 | 0.370 | 0.529 | 0.101 | 1.5436 | 1.5266 | 1.7440 |
| 50.43 | 0.469 | 0.407 | 0.124 | 0.385 | 0.495 | 0.120 | 1.5396 | 1.5257 | 1.9214 |
| 50.59 | 0.265 | 0.560 | 0.175 | 0.341 | 0.543 | 0.116 | 2.4002 | 1.2090 | 1.3051 |
| 50.60 | 0.270 | 0.555 | 0.175 | 0.320 | 0.527 | 0.153 | 2.2144 | 1.1826 | 1.7175 |
| 50.60 | 0.289 | 0.517 | 0.194 | 0.335 | 0.517 | 0.148 | 2.1639 | 1.2457 | 1.5001 |
| 50.89 | 0.538 | 0.344 | 0.118 | 0.406 | 0.483 | 0.111 | 1.3842 | 1.7353 | 1.8405 |
| 51.00 | 0.650 | 0.300 | 0.050 | 0.435 | 0.500 | 0.065 | 1.2185 | 2.0554 | 2.5413 |
| 51.10 | 0.611 | 0.310 | 0.079 | 0.512 | 0.404 | 0.084 | 1.5153 | 1.6044 | 2.0816 |
| 51.15 | 0.207 | 0.555 | 0.238 | 0.335 | 0.522 | 0.143 | 2.9455 | 1.1593 | 1.1590 |
| 51.17 | 0.315 | 0.431 | 0.254 | 0.377 | 0.446 | 0.177 | 2.1742 | 1.2649 | 1.3457 |
| 51.25 | 0.398 | 0.363 | 0.239 | 0.400 | 0.405 | 0.195 | 1.8181 | 1.3603 | 1.5728 |
| 51.31 | 0.461 | 0.309 | 0.230 | 0.424 | 0.376 | 0.200 | 1.6577 | 1.4811 | 1.6750 |
| 51.32 | 0.184 | 0.584 | 0.232 | 0.327 | 0.532 | 0.141 | 3.2106 | 1.1078 | 1.1648 |
| 51.35 | 0.573 | 0.291 | 0.136 | 0.432 | 0.422 | 0.146 | 1.3540 | 1.7647 | 2.0685 |
| 51.39 | 0.153 | 0.619 | 0.228 | 0.312 | 0.561 | 0.127 | 3.6733 | 1.0995 | 1.0643 |
| 51.45 | 0.708 | 0.282 | 0.010 | 0.450 | 0.536 | 0.014 | 1.1317 | 2.3122 | 2.6998 |
| 51.50 | 0.606 | 0.301 | 0.093 | 0.640 | 0.276 | 0.084 | 1.8682 | 1.1183 | 1.7605 |
| 51.60 | 0.075 | 0.790 | 0.135 | 0.268 | 0.656 | 0.076 | 6.3784 | 1.0005 | 1.0660 |
| 51.70 | 0.371 | 0.335 | 0.294 | 0.406 | 0.366 | 0.228 | 1.9408 | 1.3116 | 1.4710 |
| 51.75 | 0.183 | 0.516 | 0.301 | 0.347 | 0.470 | 0.183 | 3.3602 | 1.0915 | 1.1483 |
| 51.91 | 0.267 | 0.387 | 0.346 | 0.385 | 0.385 | 0.230 | 2.5356 | 1.1856 | 1.2501 |
| 51.94 | 0.529 | 0.255 | 0.216 | 0.441 | 0.343 | 0.216 | 1.4597 | 1.6032 | 1.8855 |
| 52.18 | 0.464 | 0.284 | 0.252 | 0.438 | 0.296 | 0.266 | 1.6373 | 1.2312 | 1.9710 |
| 52.26 | 0.625 | 0.201 | 0.174 | 0.468 | 0.317 | 0.215 | 1.2908 | 1.8608 | 2.3077 |
| 52.43 | 0.527 | 0.188 | 0.285 | 0.458 | 0.261 | 0.281 | 1.4897 | 1.6265 | 1.8266 |
| 52.45 | 0.301 | 0.295 | 0.404 | 0.405 | 0.310 | 0.285 | 2.3102 | 1.2293 | 1.3020 |
| 52.51 | 0.581 | 0.181 | 0.238 | 0.466 | 0.265 | 0.269 | 1.3690 | 1.7113 | 2.0897 |
| 52.55 | 0.648 | 0.188 | 0.164 | 0.476 | 0.306 | 0.218 | 1.2495 | 1.9022 | 2.4587 |
| 52.66 | 0.485 | 0.186 | 0.329 | 0.431 | 0.248 | 0.321 | 1.5109 | 1.5486 | 1.7888 |
| 52.73 | 0.410 | 0.210 | 0.380 | 0.438 | 0.244 | 0.318 | 1.8099 | 1.3465 | 1.5313 |
| 52.75 | 0.645 | 0.190 | 0.165 | 0.456 | 0.319 | 0.225 | 1.1929 | 1.9483 | 2.5013 |
| 52.78 | 0.211 | 0.389 | 0.400 | 0.370 | 0.365 | 0.265 | 2.9696 | 1.0857 | 1.2070 |
| 52.80 | 0.555 | 0.153 | 0.292 | 0.468 | 0.212 | 0.320 | 1.4222 | 1.6027 | 2.0037 |
| 52.84 | 0.348 | 0.172 | 0.480 | 0.441 | 0.198 | 0.361 | 2.1384 | 1.3283 | 1.3699 |
| 52.96 | 0.605 | 0.138 | 0.257 | 0.473 | 0.212 | 0.315 | 1.3087 | 1.7678 | 2.2295 |
| 52.97 | 0.263 | 0.279 | 0.458 | 0.397 | 0.286 | 0.317 | 2.5348 | 1.1781 | 1.2532 |
| 53.05 | 0.543 | 0.125 | 0.332 | 0.485 | 0.167 | 0.348 | 1.4895 | 1.5321 | 1.9005 |
| 53.13 | 0.500 | 0.126 | 0.374 | 0.465 | 0.163 | 0.372 | 1.5476 | 1.4786 | 1.7955 |
| 53.22 | 0.335 | 0.173 | 0.492 | 0.423 | 0.199 | 0.378 | 2.0973 | 1.3102 | 1.3793 |
| 53.36 | 0.600 | 0.110 | 0.290 | 0.471 | 0.167 | 0.362 | 1.2922 | 1.7226 | 2.2367 |
| 53.44 | 0.660 | 0.094 | 0.246 | 0.500 | 0.155 | 0.345 | 1.2405 | 1.8674 | 2.5110 |
| 53.53 | 0.760 | 0.160 | 0.080 | 0.505 | 0.349 | 0.146 | 1.0787 | 2.4732 | 3.2743 |
| 53.57 | 0.067 | 0.683 | 0.250 | 0.249 | 0.607 | 0.144 | 6.0877 | 1.0023 | 1.0168 |
| 53.57 | 0.735 | 0.137 | 0.128 | 0.512 | 0.271 | 0.217 | 1.1303 | 2.2369 | 3.0334 |
| 53.58 | 0.557 | 0.086 | 0.357 | 0.453 | 0.154 | 0.393 | 1.3278 | 2.0157 | 1.9544 |
| 53.58 | 0.411 | 0.099 | 0.490 | 0.453 | 0.118 | 0.429 | 1.8011 | 1.3409 | 1.5531 |
| 53.60 | 0.761 | 0.164 | 0.075 | 0.637 | 0.260 | 0.103 | 1.3482 | 1.8018 | 2.4838 |
| 53.64 | 0.320 | 0.127 | 0.553 | 0.429 | 0.151 | 0.420 | 2.1869 | 1.3349 | 1.3431 |
| 53.65 | 0.708 | 0.075 | 0.217 | 0.519 | 0.131 | 0.350 | 1.1883 | 1.9649 | 2.8698 |
| 53.74 | 0.232 | 0.174 | 0.594 | 0.374 | 0.187 | 0.439 | 2.6269 | 1.2020 | 1.2987 |
| 53.80 | 0.593 | 0.047 | 0.360 | 0.476 | 0.078 | 0.446 | 1.2979 | 1.8534 | 2.1829 |
| 53.81 | 0.365 | 0.090 | 0.545 | 0.435 | 0.110 | 0.455 | 1.9305 | 1.3639 | 1.4673 |
| 53.97 | 0.239 | 0.086 | 0.675 | 0.416 | 0.094 | 0.490 | 2.8048 | 1.2126 | 1.2668 |
| 54.00 | 0.421 | 0.054 | 0.525 | 0.451 | 0.064 | 0.485 | 1.7205 | 1.3138 | 1.6133 |
| 54.13 | 0.302 | 0.065 | 0.633 | 0.438 | 0.074 | 0.488 | 2.3176 | 1.2566 | 1.3394 |
| 54.13 | 0.816 | 0.170 | 0.014 | 0.552 | 0.416 | 0.032 | 1.0653 | 2.7306 | 4.0414 |
| 54.30 | 0.759 | 0.108 | 0.133 | 0.534 | 0.226 | 0.240 | 1.1047 | 2.3104 | 3.1509 |
| 54.43 | 0.176 | 0.154 | 0.670 | 0.375 | 0.165 | 0.460 | 3.3683 | 1.1713 | 1.1780 |
| 54.45 | 0.242 | 0.076 | 0.682 | 0.429 | 0.084 | 0.487 | 2.7938 | 1.2073 | 1.2266 |
| 55.00 | 0.126 | 0.197 | 0.677 | 0.377 | 0.191 | 0.432 | 4.6074 | 1.0409 | 1.0744 |
| 55.26 | 0.122 | 0.117 | 0.761 | 0.390 | 0.120 | 0.490 | 4.8704 | 1.0911 | 1.0741 |

Table II (Continued)

| temp, ${ }^{\circ} \mathrm{C}$ | $x_{1}$ | $x_{2}$ | $x_{3}$ | $y_{1}$ | $y_{2}$ | $y_{3}$ | $\gamma_{1}$ | $\gamma_{2}$ | $\gamma_{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 55.31 | 0.824 | 0.124 | 0.052 | 0.660 | 0.247 | 0.093 | 1.1954 | 2.1426 | 3.0544 |
| 55.55 | 0.133 | 0.129 | 0.738 | 0.365 | 0.140 | 0.495 | 4.1334 | 1.1437 | 1.1067 |
| 55.56 | 0.763 | 0.019 | 0.218 | 0.588 | 0.038 | 0.374 | 1.1453 | 2.1156 | 2.8684 |
| 55.96 | 0.833 | 0.072 | 0.095 | 0.604 | 0.175 | 0.221 | 1.0555 | 2.5476 | 3.8562 |
| 56.07 | 0.800 | 0.014 | 0.186 | 0.584 | 0.033 | 0.383 | 1.0612 | 2.4520 | 3.3819 |
| 56.14 | 0.847 | 0.105 | 0.048 | 0.732 | 0.188 | 0.080 | 1.2419 | 1.8799 | 2.7822 |
| 56.40 | 0.075 | 0.249 | 0.676 | 0.314 | 0.247 | 0.439 | 6.0819 | 1.0179 | 1.0401 |
| 57.61 | 0.884 | 0.082 | 0.034 | 0.742 | 0.178 | 0.080 | 1.1317 | 2.1743 | 3.7379 |
| 58.47 | 0.902 | 0.039 | 0.059 | 0.701 | 0.112 | 0.187 | 1.0119 | 2.7869 | 4.8607 |
| 58.98 | 0.068 | 0.042 | 0.890 | 0.327 | 0.045 | 0.628 | 6.2716 | 1.0111 | 1.0351 |
| 61.23 | 0.950 | 0.025 | 0.025 | 0.823 | 0.086 | 0.091 | 1.0009 | 3.0800 | 5.1489 |
| 62.32 | 0.965 | 0.010 | 0.025 | 0.912 | 0.046 | 0.042 | 1.0425 | 4.0003 | 2.3106 |

Table III. Vapor Pressure Constants (12)

| compound | $\alpha_{i}$ | $\beta_{i}$ | $\delta_{i}$ |
| :--- | :---: | :--- | :--- |
| methanol | 7.89750 | 1474.08 | 229.13 |
| 1,1-dichloroethane | 6.98530 | 1171.42 | 228.12 |
| propyl bromide | 6.91065 | 1194.889 | 225.51 |

Table IV. Redlich-Kister Correlation of Binary and Ternary Data

| system | $B_{i j}$ | $C_{i j}$ | $D_{i j}$ | rmsd |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\gamma_{1}$ | $\gamma_{2}$ |
| methanol (1)- | 1.6315 | -0.38290 | 0.22779 | 0.220 | 0.104 |
| 1,1-dichloroethane (2) |  |  |  |  |  |
| methanol (1)propyl bromide (3) | 1.7884 | -0.33412 | 0.51777 | 0.478 | 0.247 |
| 1,1-dichloroethane (2)propyl bromide (3) | 0.11295 |  |  | 0.039 | 0.056 |
| system |  | $C_{1}$ | overall rmsd |  |  |
|  |  | $\gamma$ | $y$ |  |
| methanol (1)-acetonitrile (2) propyl bromide (3) |  |  | 0 | 0.829 | $\begin{aligned} & 0.0458 \\ & 0.0465 \end{aligned}$ |  |
|  |  | -0.47348 | 0.815 |  |  |

where the constants are reported in Table III. The molar virial coefficients $B_{\eta}$ and the mixed coefficient $B_{l j}$ were calculated by the method of Tsonopoulos (4) using the molecular parameters suggested by the same author.

The ternary data reported in Table II were found to be thermodynamically consistent as tested by the McDermot-Ellis method (5) modified by Wisniak and Tamir (6). Two experimental points $a$ and $b$ are considered thermodynamically consistent if the following condition is fulfilled:

$$
\begin{equation*}
D<D_{\max } \tag{4}
\end{equation*}
$$

The local deviation $D$ is given by

$$
\begin{equation*}
D=\sum_{l=1}^{N}\left(x_{l \mathrm{a}}+x_{l \mathrm{~b}}\right)\left(\ln \gamma_{l \mathrm{~b}}-\ln \gamma_{l \mathrm{a}}\right) \tag{5}
\end{equation*}
$$

where $N$ is the number of components and

$$
\begin{align*}
& D_{\max }= \\
& \qquad \begin{array}{r}
\sum_{l=1}^{N}\left(x_{l \mathrm{a}}+x_{i \mathrm{~b}}\right)\left(1 / x_{l \mathrm{a}}+1 / y_{l \mathrm{a}}+1 / x_{l \mathrm{~b}}+1 / y_{l \mathrm{~b}}\right) \Delta x+ \\
2 \sum_{i=1}^{N}\left|\ln \gamma_{l \mathrm{~b}}-\ln \gamma_{l \mathrm{a}}\right| \Delta x+\sum_{l=1}^{N}\left(x_{l \mathrm{a}}+x_{l \mathrm{~b}}\right) \Delta P / P+\sum_{l=1}^{N}\left(x_{/ \mathrm{a}}+\right. \\
\left.\left.x_{i \mathrm{~b}}\right) \beta_{l} \mid\left(t_{\mathrm{a}}+\delta_{l}\right)^{-2}+\left(t_{\mathrm{b}}+\delta_{l}\right)^{-2}\right\} \Delta t
\end{array}
\end{align*}
$$

The errors in the measurements $\Delta x, \Delta P$, and $\Delta t$ were as previously indicated. The first term in eq 6 was the dominant one. The activity coefficients were correlated by the following Redlich-Kister expansion (7)

$$
\begin{gather*}
\text { In } \gamma_{1}=x_{2} x_{3}\left[\left(B_{12}+B_{13}-B_{23}\right)+C_{12}\left(2 x_{1}-x_{2}\right)+\right. \\
C_{13}\left(2 x_{1}-x_{3}\right)+2 C_{23}\left(x_{3}-x_{2}\right)+ \\
D_{12}\left(x_{1}-x_{2}\right)\left(3 x_{1}-x_{2}\right)+D_{13}\left(x_{1}-x_{3}\right)\left(3 x_{1}-x_{2}\right)- \\
\left.3 D_{23}\left(x_{3}-x_{2}\right)^{2}+C_{1}\left(1-2 x_{1}\right)\right]+ \\
x_{2}^{2}\left[B_{12}+C_{12}\left(3 x_{1}-x_{2}\right)+D_{12}\left(x_{1}-x_{2}\right)\left(5 x_{1}-x_{2}\right)\right]+ \\
x_{3}^{2}\left[B_{13}+C_{13}\left(3 x_{1}-x_{3}\right)+D_{13}\left(x_{1}-x_{3}\right)\left(5 x_{1}-x_{3}\right)\right] \text { (7) } \tag{7}
\end{gather*}
$$

where $B_{i j}, C_{i j}$, and $D_{i j}$ are the binary constants and $C_{1}$ is a ternary constant. The equations for two other activity coefficients were obtained by cyclic rotation of the indexes. The binary data used for calculating the binary constants were reported elsewhere $(8,9)$.

The binary and ternary Redlich-Kister coefficients were obtained by a Simplex optimization technique and are reported in Table IV. The relative values of the root mean square deviation and the ternary constant $C_{1}$ suggest that ternary data can be predicted directly from the binary systems.
Boiling points of the binary and ternary systems were correlated by the equation suggested by Wisniak and Tamir (10):

$$
\begin{equation*}
\left.T=\sum_{j=1}^{2} x_{1} T_{1}^{0}+x_{1} x_{2} \sum_{k=0}^{1} C_{k}\left(x_{1}-x_{j}\right)^{k}+\ldots\right] \tag{8}
\end{equation*}
$$

$$
\begin{align*}
& T=\sum_{i=1}^{3} x_{1} T_{1}^{0}+\sum_{\mid j=1}\left\{x_{i} x_{j} \sum_{k=0}^{1} C_{k}\left(x_{1}-x_{j}\right)^{k}\right\}+ \\
& \quad x_{1} x_{2} x_{3}\left\{A+B\left(x_{1}-x_{2}\right)+C\left(x_{1}-x_{3}\right)+D\left(x_{2}-x_{3}\right)+\ldots\right\} \tag{9}
\end{align*}
$$

$T_{i}{ }^{0}$ is the boiling point of the pure component in K and $i$ is the number of terms in the series expansion of $\left(x_{1}-x_{j}\right)$. $\mathcal{C}_{k}$ are the binary constants where $A, B, C, D$ are ternary constants. The various constants are reported in Table V , which also contains information indicating the degree of goodness of the correlation.

The boiling temperature of the mixture was correlated solely with the liquid composition by the following equation which has

Table V. Correlation of Boiling Points, Eq 8 and 9

| system | $C_{0}$ | $C_{1}$ | $C_{2}$ | $C_{3}$ | rmsd | diff $\%^{a}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| methanol (1)-1,1-dichloroethane (2) | -45.370 | -14.962 | -62.648 | 27.211 | 0.67 | 1.0 |  |  |  |
| methanol (1)-propyl bromide (3) | -49.552 | 6.9473 | -87.823 | 45.215 | 0.97 | 1.1 |  |  |  |
| 1,1-dichloroethane (2)-propyl bromide (3) | -5.7398 | -4.9563 | 0.0 | -1.8268 | 0.14 | 0.2 |  |  |  |
| system | $A$ |  |  |  |  |  |  |  |  |
| methanol (1)-acetonitrile (2)-propyl bromide | -32.203 | 114.00 | 218.25 | 0.607 | 0.91 |  |  |  |  |

${ }^{a}$ Diff $\%=(100 / n) \sum_{i=1}^{n}\left(\mid T_{\text {erptl }}-T_{\text {calced }} / T_{\text {expt }}\right)$.


Figure 1. Isothermals for the ternary system at 760 mmHg .

Table VI. Parameters of T-x Correlation (eq 10, $N=3$ ) for Methanol (1)-1,1-Dichloroethane (2)-Propyl Bromide (3) at $760 \mathrm{mmHg}{ }^{-1}$

| $i j$ | $A_{i j}$ | $B_{i j}$ | $C_{i j}$ | $D_{i j}$ | mean $D, \%$ | rmsd |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | -46.33 | 5.278 |  |  |  |  |
| 13 | -51.377 | 3.803 |  |  | 2.03 | 0.154 |
| 23 | -28.01 | 25.82 |  |  |  |  |
| 12 | -41.44 | 1.869 | -35.44 | 6.058 |  |  |
| 13 | -46.88 | 16.42 | -82.66 | 38.13 | 0.397 | 0.0238 |
| 23 | -21.46 | 6.750 | -25.67 | -26.67 |  |  |

${ }^{a} t_{1}{ }^{0}=64.68{ }^{\circ} \mathrm{C} ; t_{2}{ }^{0}=81.1^{\circ} \mathrm{C} ; t_{3}{ }^{0}=70.55^{\circ} \mathrm{C} . \quad D=\mid\left(T_{\text {exptl }}-\right.$ $\left.T_{\text {calcd }}\right) / T_{\text {exptul }} ;$ mean $D, \%=(100 / m) \sum D_{i}$.
been derived on the basis of the concept of "excess property" (11):
$T=$
$\sum_{i=1}^{N} x_{i} T_{j}^{0}+\sum_{i=1}^{N-1} \sum_{j=i+1}^{N} x_{i} x_{j}\left[A_{j j}+B_{i j}\left(x_{i}-x_{j}\right)+C_{i j}\left(x_{i}-x_{j}\right)^{2}+\ldots\right]$

This equation is useful for obtaining isothermals and for exploring the azeotropic behavior and distillation paths of ternary mixtures as explained in ref 11. The coefficients $A_{i j}, B_{i j}, C_{i j}$ are multicomponent parameters which are determined directly from the multicomponent data. Figure 1 reports the isothermals obtained on the basis of the parameters $A_{i j}, B_{i j}$ reported in Table VI by applying eq 10 for $N=3$. These isothermals might be used for considering possible distillation paths in ternary systems
as well as to conclude whether a ternary system exhibits azeotropic behavior.

As observed, whereas all binary systems have azeotropes, the ternary system does not exhibit a clear azeotropic behavior. It is possible that there is a ternary azeotrope very close in composition to that of the binary azeotrope between 1,1-dichloroethane and methanol. Table VI also contains the group of parameters $A_{i j}, B_{i j}, C_{i j}$ for the $T-x$ correlation (eq 10) which yield the smaller mean deviation between the calculated and observed values of $T$.

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Yehudit Reizner and Moshe Golden helped in the experimental and numerical determinations.

## Glossary

| $\begin{gathered} A_{i j}, B_{i j}, \\ \text { etc. } \end{gathered}$ | multicomponent adjustable parameters in eq 8 |
| :---: | :---: |
| $B_{i j}, B_{l j}$ | virial coefficients, eq 2 |
| $N$ | number of components |
| $P$ | total pressure, mmHg |
| $P_{i}{ }^{0}$ | vapor pressure of pure component $i, \mathrm{mmHg}$ |
| $T$ | boiling temperature of a mixture, K |
| $T_{i}{ }^{0}$ | boiling temperature of pure component $i, \mathrm{~K}$ |
| $t$ | temperature, ${ }^{\circ} \mathrm{C}$ |
| $x_{i}, y_{i}$ | mole fraction of component $i$ in the liquid and vapor phases |
| $\alpha_{i}$ | coefficient, Antoine equation |
| $\beta$ | coefficient, Antoine equation |
| $\gamma_{i}$ | activity coefficient of component $i$ |
| $\delta_{I}$ | coefficient, Antoine equation |

Registry No. Methanol, 67-56-1; 1,1-dichloroethane, 75-34-3; propyl bromide, 106-94-5.

## Literature Cited

(1) Boubilikova, L.; Lu, B. C. Y. J. Appl. Chem. 1969, 19, 89.
(2) Wisniak, J.; Tamir, A. J. Chem . Eng. Data 1975, 20, 168.
(3) Van Ness, H. C.; Abbott, M. M. Class/cal Thermodynamics of Nonelectrolyte Solutions; McGraw-Hill: New York, 1982.
(4) Tsonoupoulos, C. A/ChE J 1974, 33, 263.
(5) McDermott, C.; Ellis, S. R. M. Chem. Eng. Sci. 1965, $20,293$.
(6) Wisniak, J.' Tamir, A. J. Chem. Eng. Data 1977, 22, 253
(7) Redlich, O.; Kister, A. T. Ind. Eng. Chem. 1948, 40, 345.
(8) Wisniak, J.; Tamir, A. J. Chem. Eng. Data 1985, 30, 339
(9) Tamir, A., Wisniak, J. J. Chem. Eng. Data 1986, 31, 383
(10) Wisniak, J.i Tamir, A. Chem. Eng. Scl. 1975, 30, 335.
(11) Tamir, A. Chem. Eng. Scl. 1981, 36, 1453.
(12) TRC Tables. Selected Values of Properties of Chemical Components; Thermodynamics Research Center Data Project: College Station, TX, 1974.
(13) Perry, R. H. Perry's Chemical Engineers' Handbook, 6th ed.; McGrawHill: New York, 1984; p 3-58.

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# Association Effects in the Methanol-1-Pentanol System 

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> New vapor-liquid equillbria for the title system have been determined at 760 mmHg . The methanol-1-pentanol system shows strong positive deviations from Ideal behavior, and thermodynamic consistency can only be explained on the basis of thermal effects and that methanol assoclates in the vapor phase. The boliling points were well correlated with the composition of the liquid phase.

The only literature reference to the title system is that of Hill and Van Winkle (1) who reported data on the vapor-liquid in different methanol-alcohol binary systems.

Inspection of the activity coefficients reported by Hill and Van Winkle indicates that they are not thermodynamically consistent and also that there are substantial numerical errors in the conversion of weight composition to molar composition. The Dechema Data Series (2) are also in error since they report the original data in molar terms, without correcting the mistakes.

